

M035	A	PBM035A	Buffalo-Rochester	WirelessCo, L.P.	\$18,893,000.
M035	B	PBM035B	Buffalo-Rochester	AT&T Wireless PCS Inc.	\$19,864,000.
M036	A	PBM036A	Salt Lake City	Western PCS Corporation	\$45,847,030.
M036	B	PBM036B	Salt Lake City	WirelessCo, L.P.	\$46,179,852.
M037	A	PBM037A	Jacksonville	Powertel PCS Partners, L.P.	\$46,000,000.
M037	B	PBM037B	Jacksonville	PCS PRIMECO, L.P.	\$44,500,544.
M038	A	PBM038A	Columbus	AT&T Wireless PCS Inc.	\$22,290,000.
M038	B	PBM038B	Columbus	American Portable Telecommunications, Inc.	\$22,176,837.
M039	A	PBM039A	El Paso-Albuquerque	Western PCS Corporation	\$8,634,030.
M039	B	PBM039B	El Paso-Albuquerque	AT&T Wireless PCS Inc.	\$8,634,000.
M040	A	PBM040A	Little Rock	Southwestern Bell Mobile Systems, Inc.	\$12,732,501.
M040	B	PBM040B	Little Rock	WirelessCo, L.P.	\$12,321,000.
M041	A	PBM041A	Oklahoma City	Western PCS Corporation	\$11,111,111.
M041	B	PBM041B	Oklahoma City	WirelessCo, L.P.	\$13,142,346.
M042	A	PBM042A	Spokane-Billings	Poka Lambro Telephone Cooperative, Inc.	\$5,688,000.
M042	B	PBM042B	Spokane-Billings	WirelessCo, L.P.	\$6,191,000.
M043	A	PBM043A	Nashville	WirelessCo, L.P.	\$16,374,000.
M043	B	PBM043B	Nashville	AT&T Wireless PCS Inc.	\$15,810,000.
M044	A	PBM044A	Knoxville	AT&T Wireless PCS Inc.	\$10,635,000.
M044	B	PBM044B	Knoxville	BellSouth Personal Communications, Inc.	\$11,149,000.
M045	A	PBM045A	Omaha	AT&T Wireless PCS Inc.	\$4,647,000.
M045	B	PBM045B	Omaha	Cox Cable Communications, Inc.	\$5,078,000.
M046	A	PBM046A	Wichita	AT&T Wireless PCS Inc.	\$4,393,000.
M046	B	PBM046B	Wichita	WirelessCo, L.P.	\$4,901,343.
M047	A	PBM047A	Honolulu	Western PCS Corporation	\$22,361,030.
M047	B	PBM047B	Honolulu	PCS PRIMECO, L.P.	\$21,675,432.
M048	A	PBM048A	Tulsa	Southwestern Bell Mobile Systems, Inc.	\$17,562,369.
M048	B	PBM048B	Tulsa	WirelessCo, L.P.	\$16,801,654.
M049	A	PBM049A	Alaska	American Portable Telecommunications, Inc.	\$1,000,000.
M049	B	PBM049B	Alaska	GCI Communication Corp.	\$1,650,129.
M050	A	PBM050A	Guam-Northern Mariana Islands	Poka Lambro Telephone Cooperative, Inc.	\$107,000.
M050	B	PBM050B	Guam-Northern Mariana Islands	American Portable Telecommunications, Inc.	\$141,837.
M051	A	PBM051A	American Samoa	South Seas Satellite Communications Corporation	\$214,555.
M051	B	PBM051B	American Samoa	Communications International Corporation	\$228,001.

				Total Bids	\$7,019,403,797
				Total of Bid Withdrawal Penalties	\$14,836,213.
				Pioneer Preference Revenues	\$701,780,374.
			Omnipoint Corporation	\$347,518,309.	
			Cox Communications, Inc.	\$251,918,526.	
			American Personal Communications, L.P.	\$102,343,539.	
				Grand Total	\$7,736,020,384.

ATTACHMENT B
"Ownership Exhibit A " *
Direct Ownership

OMB Approval
3060-0621
Expires 10/31/97

1	2	3	4	5	6	7	8	9
Name and Address Title	Relationship	Citizenship	Principal Business	Outside Interests	Type of Interest Held	Amount Held	Percentage Held	Held on Behalf Of Name

* If applicants require additional space to respond to any Item, attach additional pages, but specify to which Exhibit and Item number those pages relate.

ATTACHMENT C
"Ownership Exhibit B" *
Indirect Ownership

OMB Approval
3060-0621
Expires 10/31/97

1	2	3	4	5	6	7	8	9	10
Name and Address Title	Relationship Name	Citizenship	Principal Business	Outside Interests	Type of Interest Held	Amount Held	Percentage Held	Held on Behalf Name	Interv. Interest

* If applicants require additional space to respond to any Item, attach additional pages, but specify to which Exhibit and Item number those pages relate .

APPENDIX B

Sample Electromagnetic Energy Emissions Calculations

Compliance with ANSI/IEEE RF Guidelines

A. Calculation of Maximum Permissible Exposure (MPE)

The IEEE C95.1-1991 guidelines for "uncontrolled" environments specify that power densities (as averaged over any 30 minute period) in the frequency range from 300-3000 MHz should not exceed values defined by the equation:

$$S = \frac{f}{1500}$$

Where:

S = Power density in milliwatts per square centimeter
(mW/cm²)
f = Frequency in MHz

For example, at a frequency of 1850 MHz the allowed power density would be $1850/1500 = 1.23 \text{ mW/cm}^2$.

Exposure of the user of a hand-held PCS transmitter must be evaluated in terms of the specific absorption rate (see part B below).

In all other cases, to determine the appropriate separation distance from a PCS transmitter to meet the MPE "uncontrolled" limits the following equation can be used.

$$S = \frac{P \times G}{4 \times \pi \times D^2}$$

Where:

S = Allowed power density
P = Power supplied to the antenna
G = Antenna gain (numeric) relative to an isotropic antenna
D = Minimum separation distance for continuous exposure

Solving for D:

$$D = \sqrt{\frac{P \times G}{4 \times \pi \times S}}$$

B. Exposure Evaluation for Hand-held PCS Transmitters

Section 4.2 of the ANSI/IEEE guidelines specifies criteria for evaluation of the exposure to users of hand-held, low-powered devices. The guidelines are given in terms of either power radiated from a device or specific absorption rate (SAR) caused by the device. Radiated power exclusions apply for operating frequencies between 100 kHz and 1500 MHz but do not apply when the device is maintained within 2.5 cm of the body of the user.

Until such time as it is decided that radiated power exclusions can be applied at frequencies above 1500 MHz (see footnote 139 in the text), compliance for a hand-held device operating at PCS frequencies between 1850 and 2200 MHz will require evaluation of the SAR produced by the device (see footnote 140).

The ANSI/IEEE guidelines specify that in "uncontrolled" environments, and for operating frequencies between 100 kHz and 6 GHz, compliance requires that spatial peak SAR not exceed 1.6 watts/kilogram (W/kg) as averaged over any 1 gram of tissue and as averaged over the appropriate time period defined in the standard. In the hands, wrists, feet and ankles spatial peak SAR shall not exceed 4 W/kg as averaged over any 10 grams of tissue.

APPENDIX C

Sample PCS/OFS Interference Calculations

A Procedure for Calculating PCS Signal Levels at Microwave Receivers

The new Rules adopted in Part 99 stipulate that estimates of interference to fixed microwave operations from a PCS operation will be based on the sum of signals received at a microwave receiver from the PCS operation. This appendix describes a procedure for computing this PCS level.

In general, the procedure involves four steps:

1. Determine the geographical coordinates of all microwave receivers operating on co-channel and adjacent frequencies within the coordination distance of each base station and the characteristics of each receiver, i.e., adjacent channel susceptibility, antenna gain, pattern and height, and line and other losses.
2. Determine an equivalent isotropically radiated power (e.i.r.p.) for each base station and equivalent e.i.r.p. values for the mobiles and portables associated with each base station. Determine the values of pertinent correction and weighting factors based on building heights and density and distribution of portables. Close-in situations, prominent hills, and extra tall buildings require special treatment.
3. Based on PCS e.i.r.p. values, correction and weighting factors, and microwave receiving system characteristics determined above, calculate the total interference power at the input of each microwave receiver, using the Longley-Rice propagation model.
4. Based on the interference power level computed in step 3, determine interference to each microwave receiver using criteria described in Part 99 and EIA/TIA Bulletin 10E.

The interference from each base station and the mobiles and portables associated with it is calculated as follows:

$$P_{rbi} = 10\log(P_{tbi}) - L_{bi} - UC_i + G_{mwi} - AC_i$$

$$P_{rmi} = 10\log(n_{mi} \times P_{tmi}) - L_{mi} - UC_i + G_{mwi} - AC_i$$

$$P_{rpsi} = 10\log(n_{psi} \times P_{tpsi}) - L_{psi} - UC_i + G_{mwi} - AC_i$$

$$P_{rpbi} = 10\log(n_{pbi} \times P_{tpbi}) - L_{pbi} - UC_i - (BP_i - BH_i) + G_{mwi} - AC_i$$

$$P_{rpri} = 10\log(n_{pri} \times P_{tpri}) - L_{pri} - (UC_i - BH_i) + G_{mwi} - AC_i$$

where:

P refers to Power in dBm - B1 -

p refers to power in milliwatts

P_{rbi} = Power at MW receiver from i th base station in dBm
 P_{tbi} = e.i.r.p. transmitted from i th base station in milliwatts,
 which equals power per channel x number of channels x
 antenna gain with respect to an isotropic antenna -
 line loss
 L_{bi} = Path loss between MW and base station site in dB
 UC_i = Urban correction factor in dB
 G_{mwi} = Gain of MW antenna in pertinent direction (dBi)
 AC_i = Adjacent channel discrimination of MW system in dB
 P_{rmi} = Power at MW receiver from mobiles associated with i th
 base station
 P_{tmi} = e.i.r.p. transmitted from mobiles associated with i th
 base station
 n_{mi} = Number of mobiles associated with i th base station
 L_{mi} = Path loss between MW and mobile transmitters in dB
 P_{rpsi} = Power at MW receiver from outdoor portables (s for
 sidewalk)
 P_{tpsi} = e.i.r.p. transmitted from outdoor portables associated
 with i th base station
 n_{psi} = Number of outdoor portables associated with i th base
 station
 L_{psi} = Path loss between MW and outdoor portables in dB
 P_{rpbi} = Power at MW receiver from indoor portables (b for
 building)
 P_{tpbi} = e.i.r.p. transmitted from indoor portables associated
 with i th base station
 n_{pbi} = number of indoor portables associated with i th base
 station
 L_{pbi} = Path loss in dB between MW and base station site (using
 average building height divided by 2 as effective antenna
 height)
 P_{rpri} = Power at MW receiver from rooftop portables (r for
 rooftop)
 P_{tpri} = e.i.r.p. transmitted from rooftop portables associated
 with i th base station
 n_{pri} = Number of rooftop portables associated with i th base
 station
 L_{pri} = Path loss in dB between MW and base station site (using
 average building height as effective antenna height)
 BP_i = Building penetration loss at street level in dB
 BH_i = Height gain for portables in buildings dB = $2.5 \times (nf-1)$,
 where nf is number of floors

Finally, the total PCS interference power at a given microwave receiver from all the base stations in a given frequency band is found by summing the contributions from the individual stations. Likewise, the total interference power at a given microwave receiver from all mobiles and portables operating in a given frequency band is found by summing the contributions from the mobiles and portables associated with each cell.

$$P_{rb} = \sum_i P_{rbi} \quad \text{milliwatts}$$

$$P_{rm} = \sum_i (P_{rmi} + P_{rpsi} + P_{rpbi} + P_{rpri}) \quad \text{milliwatts}$$

$$P = 10 \log(p) \quad \text{dBm}$$

Base Stations. Interference from each base station to each microwave should normally be considered independently. A group of base stations having more or less (within ± 50 percent) the same height above average terrain, the same e.i.r.p., basically the same path to a microwave receiving site, and subtending an angle to that receiving site of less than 5 degrees, may be treated as a group, using the total power of the group and the average antenna height of the group to calculate path loss, L.

The urban correction factor, UC, should not be applied to base station antenna heights that are greater than 50 percent of the average building height for a cell.

Mobile Stations. The e.i.r.p. from mobile transmitters is weighted according to the number of base station channels expected to be devoted to mobile operation at any given time. The antenna height of mobiles used in calculating path loss, L, is assumed to be 5 feet.

Portable Stations. The e.i.r.p. from the portable units associated with each base station is weighted according to the estimated portion of portables associated with that cell expected to be operated inside buildings at any given time and the portion which could be expected to be operating from elevated locations, such as balconies or building rooftops. For example, in the case of service intended for business use in an urban area, one might expect that perhaps 85 percent of the portables in use at any given time would be operating from within buildings and perhaps 5 percent might be operating from rooftops or balconies. The remaining 10 percent would be outside at street level.

Calculation of an equivalent e.i.r.p. for cells in suburban areas will involve different weighting criteria. Contributions to the e.i.r.p. from that portion of portables within a cell operating from inside single-family homes shall be reduced by 10 dB.

Urban Correction Factor. The urban correction factor (UC) depends on the height and density of buildings surrounding a base station. For the core area of large cities, it is assumed to be 35 dB. For medium size cities and fringe areas of large cities (4- to 6-story buildings with scattered taller buildings and lower buildings and open spaces) it is assumed to be 25 dB; for small cities and towns, 15 dB, and for suburban residential areas (one- and two-story, single family houses with scattered

multiple-story apartment buildings, shopping centers and open areas), 10 dB.

Building Height and Building Penetration Factors. The building height correction, BH, is a function of the average building height within the nominal coverage area of the base station. It is used in conjunction with the building penetration loss, BP, to adjust the expected interference contribution from that portion of the portables transmitting from within buildings. The adjustment is given by:

BP = 20 dB in urban areas

BP = 10 dB in suburban areas

$BH = 2.5 \times (nf - 1) \text{ dB}$

where nf is the average height (number of floors) of the buildings in the area.

(Note that this formula implies a net gain when the average building height is greater than 8 floors). All buildings more than twice the average height should be considered individually. The contribution to BH from that portion of portables in the building above the average building height should be increased by a factor of $20\text{Log}(h)$ dB, where h is the height of the portables above the average building height in meters.

Adjacent Channel Correction Factor. A factor based on the selectivity of the microwave receiver.

Propagation Model. The PCS to microwave path loss, L, is calculated using the Longley-Rice propagation model, Version 1.2.2., in the point-to-point mode. The Longley-Rice [1] model was derived from NBS Technical Note 101 [3], and updated in 1982 by Hufford [3]. Version 1.2.2 incorporated modifications described in a letter by Hufford [4] in 1985. Terrain elevations used as input to the model should be from the U.S. Geological Survey 3-second digitized terrain database.

Special Situations. If a cell size is large compared to the distance between the cell and a microwave receiving site so that it subtends an angle greater than 5 degrees, the cell should be subdivided and calculations should be based on the expected distribution of mobiles and portables within each subdivision.

If terrain elevations within a cell differ by more than a factor of two-to-one, the cell should be subdivided and microwave interference calculations should be based on the average terrain elevation for each subdivision.

If a co-channel PCS base station lies within the main beam of a microwave antenna (± 5 degrees), there is no intervening terrain,

and the power at the microwave receiver from that base station, assuming free space propagation, would be 3 dB or less below the interference threshold, interference will be assumed to exist unless the PCS licensee can demonstrate otherwise by specific path loss calculations based on terrain and building losses.

If any part of a cell or cell subdivision lies within the main beam of a co-channel microwave antenna, there is no intervening terrain, and the accumulative power of 5 percent or less of the mobiles, assuming free space propagation would be 3 dB or less below the interference threshold, interference will be assumed to exist unless the PCS licensee can demonstrate otherwise by specific path loss calculations based on terrain and building losses.

If a building within a cell or cell subdivision lies within the main beam of a co-channel microwave antenna, there is no intervening terrain, and the cumulative power of 5 percent or fewer of the portables, assuming free space propagation, would be 3 dB or less below the interference threshold, interference will be assumed to exist unless the PCS licensee can demonstrate otherwise by specific path loss calculations based on terrain and building losses.

References:

1. Longley, A.G. and Rice, P.L., "Prediction of Tropospheric Radio Transmission Loss Over Irregular Terrain, A Computer Method-1968", ESSA Technical Report ERL 79-ITS 67, Institute for Telecommunications Sciences, July 1968.
2. Hufford, G.A., Longley, A.G. and Kissick, W.A., "A Guide to the use of the ITS Irregular Terrain Model in the Area Prediction Mode", NTIA Report 82-100, U.S. Department of Commerce, April 1982. Also, Circular letter, dated January 30, 1985, from G.A. Hufford, identifying modifications to the computer program.
3. Rice, P.L., Longley, A.G., Norton, K.A., Barsis, A.P., "Transmission Loss Predictions for Tropospheric Communications Circuits," NBS Technical Note 101 (Revised), Volumes I and II, U.S. Department of Commerce, 1967.
4. Hufford, G.A., Memorandum to Users of the ITS Irregular Terrain Model, Institute for Telecommunications Sciences, U.S. Department of Commerce, January 30, 1985.

APPENDIX B

Sample Electromagnetic Energy Emissions Calculations

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Where:

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For example, at a frequency of 1850 MHz the allowed power density would be $1850/1500 = 1.23 \text{ mW/cm}^2$.

Exposure of the user of a hand-held PCS transmitter must be evaluated in terms of the specific absorption rate (see part B below).

In all other cases, to determine the appropriate separation distance from a PCS transmitter to meet the MPE "uncontrolled" limits the following equation can be used.

$$S = \frac{P \times G}{4 \times \pi \times D^2}$$

Where:

- S = Allowed power density
- P = Power supplied to the antenna
- G = Antenna gain (numeric) relative to an isotropic antenna
- D = Minimum separation distance for continuous exposure

Solving for D:

$$D = \sqrt{\frac{P \times G}{4 \times \pi \times S}}$$

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$$P_{rpri} = 10\log(n_{pri} \times P_{tpri}) - L_{pri} - (UC_i - BH_i) + G_{mwi} - AC_i$$

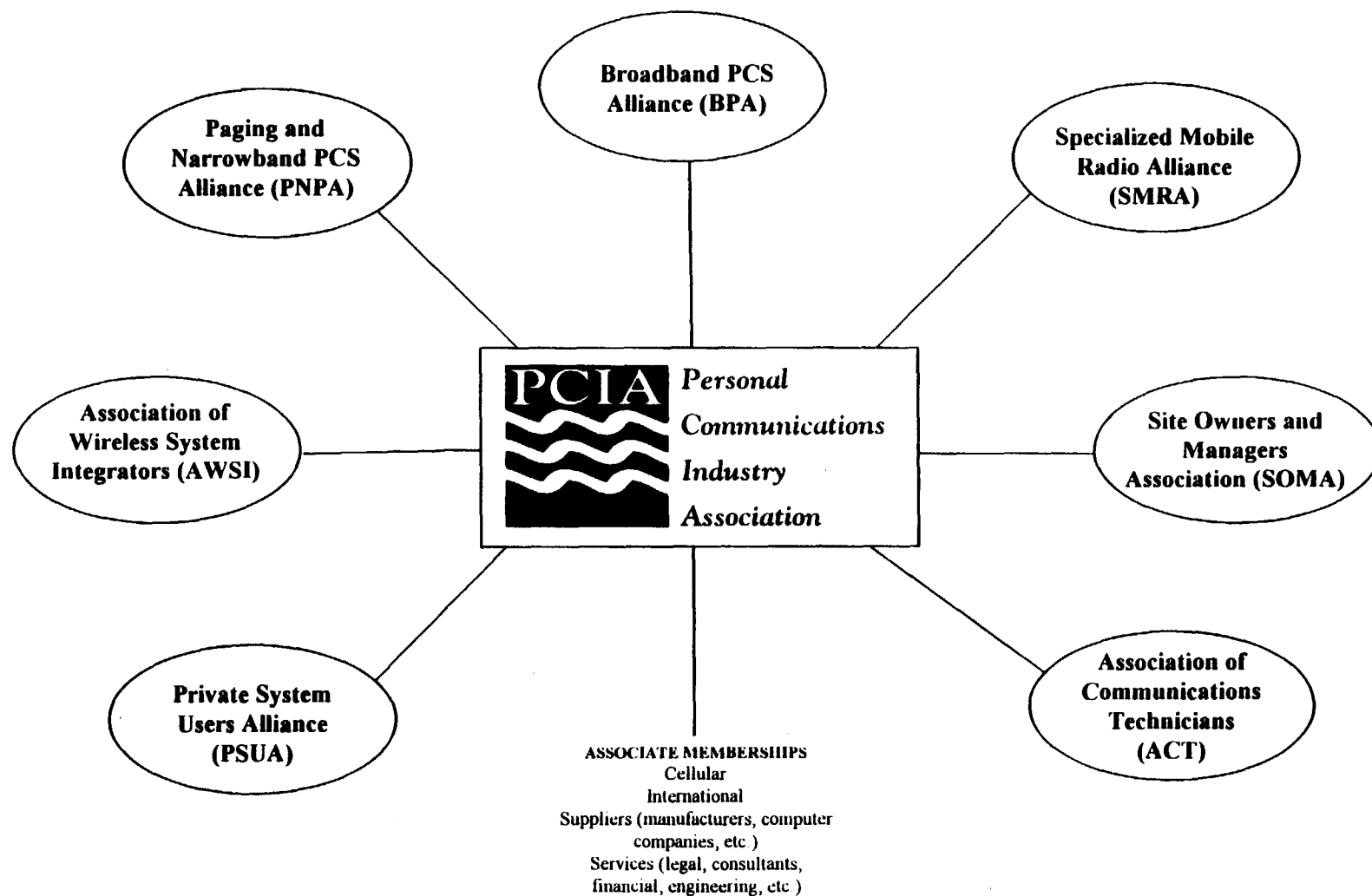
where:

P refers to Power in dBm - B1 -

p refers to power in milliwatts

PCIA's Broad, Powerful Membership Base

A Federation of Alliances



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OFFICE OF SECRETARY

**900 MHz NARROWBAND
PERSONAL COMMUNICATIONS SERVICES
REGULATORY HANDBOOK**

April 1995

Prepared By:

R. Michael Senkowski
Katherine M. Holden
Eric W. DeSilva
Lauren A. Carbaugh
WILEY, REIN & FIELDING

Counsel to PCIA

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TABLE OF CONTENTS

I.	INTRODUCTION	1
A.	Purpose of This Handbook	1
B.	PCIA and Its Objectives	2
1.	Committed to the Wireless Vision	2
2.	Creating New Opportunities	3
3.	The Voice for PCS	3
4.	Point of Contact	6
C.	Structure and Contents of Handbook	6
II.	900 MHz NARROWBAND PCS ALLOCATIONS AND MARKET STRUCTURE	7
A.	The Definition of Narrowband PCS	7
B.	Spectrum Allocations	8
C.	Service Areas	10
D.	Restrictions on Ownership/Eligibility	12
1.	The Three License Cap	12
2.	Eligibility for 12.5 kHz Talk-Back Channels	13
3.	Non-U.S. Ownership Restrictions	14
III.	900 MHz NARROWBAND PCS LICENSING RULES AND PROCEDURES . .	16
A.	Pre-Auction Application Procedures	16
1.	Initial FCC Public Notice	16
2.	Filing Short Form Applications	18

3.	Second and Third FCC Public Notices	19
4.	Upfront Payment	19
5.	Fourth Public Notice	20
B.	Conduct of the Narrowband Auctions	20
1.	Bidding Rounds	22
2.	Auction Stages	22
3.	Minimum Bid Increments	23
4.	Activity Rules	24
5.	Stopping Rules	26
6.	Penalty for Withdrawn High Bids	27
C.	Post Auction Payments and Procedures	27
1.	Down Payment	27
2.	Long Form Application	28
3.	Public Notice and Petition To Deny Procedures	28
4.	Bid Default Penalties	29
D.	Anti-Collusion Regulations	30
1.	Limitations on Bidders Prior to Filing an FCC Form 175	30
2.	Limitations on Bidders After Filing an FCC Form 175	31
3.	Consequences of Failing To Comply With Anti-Collusion Requirements	32
E.	Special Provisions Relating to Designated Entities	33
1.	Who Qualifies as a Designated Entity	33
a.	<i>Small Businesses</i>	34

b.	<i>Women and/or Minority Owned Businesses</i>	35
c.	<i>"Control Groups" and Passive Equity Arrangements</i>	36
2.	<i>Affiliation</i>	38
a.	<i>In General</i>	38
b.	<i>Directors, Officers, Key Employees, and Management</i>	39
c.	<i>Identity of Interest</i>	40
d.	<i>Stock Ownership</i>	41
e.	<i>Trusts</i>	41
f.	<i>Waiver of Affiliation</i>	41
g.	<i>Management Agreements and Joint Marketing Agreements</i>	42
3.	<i>Controlling Abuse</i>	42
4.	<i>Preferences</i>	43
a.	<i>Reduced Upfront Payments</i>	43
b.	<i>Installment Payments</i>	43
c.	<i>Bidding Credits</i>	44
d.	<i>Tax Certificates</i>	44
5.	<i>Entrepreneurs' Blocks</i>	46
IV.	<i>900 MHz NARROWBAND PCS TECHNICAL RULES</i>	47
A.	<i>Power Limits</i>	47
B.	<i>Authorized Bandwidth and Emissions Limits</i>	48
C.	<i>Coexisting With Other PCS Users</i>	49
D.	<i>Coordination in Canadian and Mexican Border Areas</i>	51

E.	PCS Equipment Type Acceptance Requirements	53
F.	PCS Numbering	55
G.	911 and E-911 Requirements	57
V.	900 MHz NARROWBAND PCS OPERATIONAL RULES AND REGULATIONS	57
A.	Federal and State Jurisdictional Relationship	57
B.	CMRS Regulations	59
1.	Obligation To Provide Service at Just and Reasonable Rates on a Non-Discriminatory Basis	61
2.	Interconnection	62
3.	Section 208 Complaint Procedures	63
4.	Telecommunications Relay Services Obligations	64
C.	Permissible Communications	65
D.	Conditions of Authorizations	66
1.	License Term and Renewal	66
2.	Build-Out Requirements	66
E.	Transfer and Assignment of PCS System Licenses	68
1.	Procedures for Transfer of Control and Assignment of Authorizations	68
2.	Ensuring Compliance With Ownership and Control Obligations	71
3.	Trafficking Considerations for Designated Entities	72
F.	Regulation of Base Station Sites and Antenna Structures	73
1.	Marking and Lighting of Antenna Structures	74
a.	<i>Federal Aviation Administration ("FAA") Requirements</i>	<i>74</i>

<i>b.</i>	<i>FCC Requirements</i>	75
2.	Environmental Impact Considerations	76
3.	Electromagnetic Energy Emissions Limits	77
4.	Local Zoning	77
G.	Privacy Considerations	78
1.	Protecting Subscriber Privacy	78
2.	Assistance to Law Enforcement	80
H.	Resale of Interstate and International Communications	82
1.	Resale of Interstate Services	83
2.	Resale of International Services	84
I.	Reporting Requirements and Regulatory Fees	86
VI.	BACKBONE MICROWAVE AUTHORIZATION PROCEDURES AND OPERATIONAL REQUIREMENTS	87
A.	Uses	87
B.	Application Procedures and Prior Coordination Procedures	87
C.	License Term	89
D.	Temporary Fixed Authority and Blanket Special Temporary Authority	89
VII.	CONCLUSION	90
App. A --	Summary of FCC Forms and Fees	A1
App. B --	Sample Electromagnetic Energy Emissions Calculations	B1

INDEX TO FIGURES

Figure 1 Time Line of PCIA PCS Milestones 4

Figure 2 PCIA Membership by Industry Sector 5

Figure 3 Relationship Between Narrowband PCS Allocations 9

Figure 4 MTA and Regional License Territories 11

Figure 5 Flow Chart of the Narrowband PCS Application Process 17

INDEX TO TABLES

Table 1	Narrowband PCS Channel Summary	8
Table 2	900 MHz Narrowband PCS Regional Licenses by MTA	10
Table 3	Narrowband PCS Channel Auction Summary	22
Table 4	Required Narrowband PCS Auction Activity Levels	27
Table 5	Control Options To Qualify for Treatment as a Women-Owned or Minority-Owned Firm	37
Table 6	Proposed Bidding Preferences in Entrepreneur's Blocks	47
Table 7a	Attenuation for ≤ 10 kHz Authorized Bandwidth	49
Table 7b	Attenuation for > 10 kHz Authorized Bandwidth	50
Table 8	Narrowband PCS Height/Power Reduction Table	51
Table 9	Channel Availability in Canadian Border Areas	53
Table 10	Title II Regulations Applicable to PCS Licensees	61
Table 11	Narrowband PCS Build-Out Requirements	68
Table 12	Designated Entity Penalty Provisions for License Transfers to Non-Qualifying Entities	74

I. INTRODUCTION

A. Purpose of This Handbook

This handbook is intended to provide a comprehensive review of the regulatory ground rules, as they currently exist, imposed by the Federal Communications Commission ("FCC") for the new licensed narrowband personal communications services ("PCS") operating in the 900 MHz band. It is designed to be a reference tool for the industry participating in this new segment of the wireless, mobile communications marketplace. A companion edition, the *2 GHz Broadband Personal Communications Services Regulatory Handbook*, provides a similar overview of the regulations applicable to PCS systems operating in the 2 GHz band. PCIA has also published a *Designated Entity Handbook*, which reviews in detail the ownership limitations on designated entities seeking to bid for PCS licenses, and a *1995 Interconnection Primer*, which provides a comprehensive guide to negotiating interconnection arrangements with local telephone companies.

While this handbook is intended to be a complete and accurate review of the licensing and operational requirements governing PCS, it is not meant to serve as a substitute for the reader's own review and analysis of the applicable regulations and policies. In addition, this handbook reviews only requirements imposed at the federal level by the FCC; there also may be applicable requirements imposed by state and local regulatory bodies. More importantly, as of the date of publication of this handbook, many rules and policies affecting PCS are undergoing further review by the FCC, and information contained in this handbook may be superseded by legal or regulatory developments that occur subsequent to publication. Before

the reader undertakes any action based on the material set forth in this handbook, it is advisable to take steps to ensure that such action is based on the most current set of facts, governing laws and rules, and their interpretation.

B. PCIA and Its Objectives

1. Committed to the Wireless Vision

Whether your company offers paging, cellular, data or any other form of communications services, the key concept of "personalized communications" will drive your business in the communications world of the future. As the wireless communications industry continues to target the mass market, knowing what the consumer wants and needs and developing personalized services to meet those needs will be vital to success.

Established in 1949, the Personal Communications Industry Association (formerly Telocator) is the leading national trade association for companies in the PCS industry. Since its inception, PCIA has been instrumental in advancing regulatory policies, legislation and technological standards that have helped launch the age of personal communications services.

One of PCIA's greatest strengths is its ability to foster and to represent consensus in order to advance the interests of the PCS industry. Through market forecasts, publications, committees, and its annual convention -- the Personal Communications Showcase -- PCIA is committed to maintaining its position as the association for the PCS industry.